configuration requirement imposed by item (ii), brings out that there are no restrictions on wall angle of articulated topographical definition. The distended condition of the strip called for by claims 1 and 11, as amended, is shown in Figs. 2-4 of the drawings. Claim 11 (and claims 12-13 dependent thereon), as amended, now requires a combination of unique features, namely, (i) that the article comprises a plurality of self-nesting amorphous metal alloy strips; (ii) that each of the strips is a generally planar, previously cast amorphous metal strip; (iii) that each strip has an articulated topographical definition at a depth greater than the strip thickness; (iv) that the articulated topographical definition is produced on each of the strips by application of selected forces; and (v) that application of the selected forces induces permanent deformation of a shape or configuration distending at a depth greater than the strip thickness without strip embrittelement. Each of these amendments is clearly supported by the original specification. A redline document highlighting the amendments to the claims and an unmarked (clean) copy of the amended claims are enclosed herewith.

As pointed out by the original specification, the articulated topographical definitions are created by the application of selected forces to a generally planar ("2-dimensonal") amorphous metal foil or ribbon in order to introduce permanent deformations therein so to produce a non-planar ("3-dimensional") amorphous metal foil or ribbon which includes a geometric pattern, texture, profile or other feature, collectively referred to as "articulated topographical definitions". With respect to such articulated topographical definitions, it is required only that there be introduced permanent deformations which will <u>distort or distend the generally planar amorphous metal foil or ribbon</u>, as is usually <u>applied in an "as cast" form</u>, so to provide a permanent non-planar three-dimensional profile. The specification also teaches that the geometrically repeating articulated topographical definitions can be <u>any shape or configuration</u> which provides a regularly repeating

pattern of articulated topographical definitions, and ideally are those shapes or configurations which show an interlock between their individual patterns. Further, the specification discloses that the selection of an appropriate deformation temperature is to be based on the considerations of minimizing or eliminating crystallization during the stamping step, and ideally also based on the considerations of minimizing or eliminating embrittlement of the amorphous metal foil during this stamping step. The original specification clearly points out that the temperature at which the plastic deformation is carried out is a critical factor. With regard to the temperature at which the stamping process occurs, applicants have discovered that while a higher elevated temperature typically results in a shorter residence time in the die, or alternately less pressure required of the die, such elevated temperature is not desired where there is a significant risk of crystallization and/or of embrittlement of the amorphous metal alloy foil or strip. The protrusions and depressions are large, as compared to the strip thickness and can have a selected shape or configuration (see also Figs. 2-4). As a result, the protrusions nest or interlock with depressions of an adjoining strip to create laminations. This relationship is discussed at page 4, line 9 of the specification. In addition, the tips of the protrusions of a plastically deformed flat sheet can be lopped off. With this arrangement, there is created a cutting edge for an abrading tool (see page 11, line 29 of the specification). These protrusions and depressions are typically created by subjecting a previously cast planar sheet of cast amorphous metal to plastic deformation forces provided by a male/female die set. (See page 15, lines 13-21 of the specification). The restriction "of a shape or configuration distending " and "without strip embrittelement or crystallization" is fully supported by page 5, line 1, page 8, line 22-29, of the original specification. Such articulated topographical definitions are created by the application of selected forces to a generally planar (2-dimensonal) amorphous metal foil or ribbon. These selected forces introduce permanent deformations in the ribbon that produce a non-planar (3-dimensional)

amorphous metal foil or ribbon. Such deformations can include a geometric pattern, texture, profile or other feature, collectively referred to as "articulated topographical definitions". With respect to such articulated topographical definitions, it is required only that there be introduced permanent deformations which will distort or distend the generally planar previously cast amorphous metal foil or ribbon to provide a permanent non-planar three-dimensional profile.

There are significant advantages to creating "articulated topological definition" by plastic deformation of a flat previously cast sheet in the "as cast" condition, as compared to casting an "articulated topological definition" article by free flow of molten metal into articulations contained by the chill wheel, as disclosed by Narasimhan. Specifically, Narasimhan uses a casting chill or casting belt substrate, each of which has depressions that are replicated by the cast strip. There are serious limitations to the wall angles of protrusions created by the Narasimhan casting process, especially when the thickness of protrusions or depressions is greater than the thickness of the strip. Also, the angles of the Narasimhan protrusions are more restricted, being less than 65 degrees wall angle, when the walls are transverse to the casting direction (see col. 3, line 21 of Narasimhan). When these angular relationships are not adhered to within a 2-degree range, the protrusions do not attach to the base strip (col. 2 line 16). When protrusions are disconnected to the base strip, the Narasimhan product does not effectively function as an abrasive, since the protrusions tend to tear and fold over. In addition, the patterns produced by the direct casting process of Narasimhan have an inherent periodicity, which depends on the circumference of the chill surface; this is the case whether the chill surface is a quench-wheel or a casting belt. Arbitrary shapes, including non-periodic structures or articulations, the depressions of which have wall angle greater than 65 degrees on all sides, cannot be produced by the Narasimhan process. For the case of small wall thickness angles, the protrusions are inherently spaced further apart, and number of protrusions

available in an abrasive article produced by the Narasimhan direct casting process is severely reduced. On the other hand, protrusions formed by plastic deformation, as called for by Applicants' claims, can have any shape or configuration without any restriction on wall angles, spacing or periodicity. Unlike the Narasimhan process, amorphous metal alloy strip called for by applicants; claims has a strip thickness that is precisely preserved without any discontinuity of the protrusions at the strip base plane. It is therefore submitted that the product called for by applicants' claims has substantially different geometric features than those disclosed by Narasimhan.

There also exist significant magnetic property differences as a consequence of plastic deformation. Narasimhan's process uses a liquid metal that flows freely into depressions or protrusions provided on the chill surface. This free flow of molten liquid metal is not deformation by force, as suggested by the Examiner. Molten metal naturally takes the shape of any containment provided; this is a fundamental property of a liquid. On the other hand, plastic deformation of a previously cast, amorphous metal sheet is readily carried out at markedly different temperatures. Plastic deformation results in slip bands along which easy magnetization occurs. The "articulated topological definition" is greater than the thickness of the strip, so that magnetic domains align along the slip bands. This alignment is discussed in Amorphous Metallic Alloys, Edited by F.E. Luborsky, Pub. Butterworths, 1983, pages 313-314; see, in particular, the section entitled "Roll-Induced Anisotropy". A copy of the "Roll-Induced Anisotropy" chapter has been provided with Applicants' April 3, 2003 amendment. Clearly, the magnetic properties of the as-cast Narasimhan product are very different from those afforded by plastically deformed, previously cast strip having "articulated topological definition", as called for by applicants' amended claims 1-13. The effect of slip bands on the hardness and other mechanical properties of applicants' claimed strip is minimal.

More specifically, the product of claims 1-13, as amended, is restricted to modification of a previously produced strip in accordance with a particular process. That process requires the preparation of geometrically articulated amorphous alloys having a shape or configuration produced by applying force to permanently deform a previously cast planar, amorphous metal sheet with depressions and protrusions greater than the strip thickness without embrittelement or crystallization. It does not include products wherein the articulations are produced by direct quenching from a melt. The products, which result from application of selected forces to induce permanent deformation, produce 3-dimensional shapes in a previously cast, generally planar 2-dimensional ribbon. These geometrically articulated amorphous metal shapes are structurally relaxed due to the absence of directional thermal contraction stresses. As a result, the geometrically articulated amorphous metal shapes are endowed with superior mechanical properties, including exceptional cutting capability and excellent magnetic properties. On the other hand, as quenched products of the type produced by Narasimhan, which are said to have geometrical articulation, are in an un-relaxed state, as shown in Fig. 1 of the specification. They do not possess superior magnetic properties or cutting properties, since internal stresses are additive to applied stresses. The magnetic and mechanical properties of applicants' claimed geometrically articulated amorphous strip, which is produced by mechanical forming processes, are superior to properties produced by direct quench methods. In addition, the Narasimhan process for direct casting of angular articulation, similar to hexagonal geometrical articulation, as shown in Fig. 2A, generally results in poor reproduction due to (i) melt accumulation along angular edges and wall angle, and (ii) wall orientation with respect to strip casting direction. This melt accumulation behavior, as well as the poor reproduction of the pattern, is acknowledged by USP 4,322,848 to Narasimhan (see col. 1, line 60 through col. 2, line 17). By way of contrast, the mechanical deformation process used to modify previously cast strip

and thereby produce the geometrically articulated strip of applicants' claims does not have any of these limitations, since the metallic glass essentially flows along the shape of the die. Moreover, non-periodic structures cannot be produced by the Narasimhan process, since the geometrically articulated amorphous metal invariably has a periodicity, created by the circumference of a quench wheel or belt. Clearly, the plastic deformation of previously cast amorphous metal strip to create geometrically articulated amorphous metal alloys affords definitive advantages upon which patentability can be predicated.

Claims 1-4 and 6-9 were rejected under 35 U.S.C. 102(b) as being anticipated by or, in the alternative, under 35 U.S.C. 103(a) as being obvious over Narasimhan (U.S. Patent 4.332,848).

The Examiner has taken the position that Narasimhan discloses glassy metal strips having a composition within the limitations of instant claim 4 and which contain a repeating geometrical pattern of structurally defined protuberances and/or indentations. In addition, the Examiner has stated that the preferred depth in Narasimhan is as much as 10 times the thickness of the strip; see Narasimhan column 7, line 60. With regard to the "application if selected forces that induce permanent deformation" as claimed, Examiner has indicated that the force of the molten metal in Narasimhan hitting the contoured surface of the casting mechanism would appear to meet this limitation. With respect to claims 6-9, the Examiner's position is that the suitability of a material for abrasive or cutting purposes is directly related to its composition, shape, and relative hardness to the material being abraded or cut. Because all of these parameters are the same in the prior art or the claimed invention, the Examiner's position is that the claimed limitations are inherent in the Narasimhan material. Thus all aspects of the claimed invention appear to be fully met by Narasimhan.

The Examiner has also stated that it appears to be Applicants' intent that the claimed "forces that induce permanent deformation" are forces that the material has been subjected to subsequent to solidifying, as opposed to any forces during solidification as described in the preceding paragraph. This difference would imply a difference in the process by which the claimed products are made, as opposed to any difference between the actual products and those of Narasimhan. It is well settled that a product-by-process claim defines a product, and that when the prior art discloses a product substantially the same as that being claimed, differing only in the manner by which it is made, the burden falls to applicant to show that any process steps associated therewith result in a product materially different from that disclosed in the prior art. See In re Brown (173 USPQ 685) and In re Fessman (180 USPQ 524). In the present case, Applicant has not met this burden, and the claimed products are held to be at best obvious variants of those disclosed by Narasimhan.

The Examiner has also stated that Narasimhan discloses glassy metal strips having a composition within the limitations of claim 4, and which contain a repeating geometrical pattern of structurally defined protuberances and/ or indentations. With respect to claims 8-9, the Examiner's has taken the position that suitability of a material for abrasive or cutting purposes is directly related to the composition, shape, and relative hardness of the material being abraded or cut; since all of these parameters are the same in the prior art or the claimed invention, the claimed limitations are inherent in the Narasimhan material.

These statements of the Examiner are, respectfully, traversed. There are strong differences between the geometrically articulated 'as cast' amorphous material and that produced by permanent deformation according to the subject invention. In the process disclosed by USP 4,332,848 to Narasimhan, the chill wheel or belt is designed so that the melt can flow and replicate the wheel's shape during casting (see col. 1, lines 60 through col. 2 line 17). In that process, quench wheel

depressions have different casting velocities due to wheel radius reductions at the locations of the depressions. This causes the geometrically articulated amorphous material to have a permanent curvature akin to that of the chill wheel. If the geometrically articulated ribbons are straightened by application of force, the ribbon tears or flattens out at these geometrical articulations. Casting on a belt may, in certain cases, be devoid of these problems, which result from casting at different velocities. However, in such cases the belt would need to be extraordinarily thick to accommodate the chill surface depressions. Moreover, for such cases, the driving wheels for the belt would need to be extraordinarily large, making the process highly impracticable. As a matter of fact, amorphous strip is presently produced on a quench wheel, and not on a belt of any kind, owing to troublesome problems encountered when driving a thick belt, and problems created by fatigue of the belt surface due to thermal loading and repeated bending action. Thus, as a practical matter, non-periodic geometrical articulation cannot be produced by the quenching process, since the quench surface is periodically brought under the casting nozzle. The 'as cast' ribbons have trapped internal stresses induced during quenching. Such stresses are thermal contraction stresses that have different values along different directions of the ribbon. Mechanical properties of the ribbons are correspondingly reduced due to the additive nature of the internal stresses with applied stresses. In addition the magnetic properties are reduced owing to these internal stresses, since most magnetic alloys are magnetostrictive. There are severe restrictions on the wall angle of protrusions created during direct quenching with the Narasimhan process. Such protrusions are nominally restricted to 65 degrees to the strip basal surface, when the protrusions are larger than the strip thickness. Use of small wall angles results in larger spacing between protuberances, decreasing the number of cutting elements in an abrasive strip. Additionally, as previously noted, strip produced by the Narasimhan direct casting process is much more likely to contain discontinuities between the protrusions and the strip

surface, especially when the wall angle is slightly larger than 65 degrees by even as little as 2 degrees.

The geometrically articulated strip defined by applicants' claims 1-4 and 6-9, as amended, is clearly identifiable from an as-cast strip. Unlike an as-cast strip, the geometrically articulated strip of applicants' claims 1-4 and 6-9, as amended, exhibits (i) an absence of internal stresses; (ii) superior magnetic properties; (iii) non-periodic as well as periodic geometrical articulations of a selected shape or configuration; iv) preservation of strip flatness; and v) no restrictions on wall angle of the articulations. Significantly, the geometrical articulations called for by applicants' claims are much larger structures, having thickness greater than the thickness of the amorphous ribbon (see, for example, Fig. 2B, 3B and 4 of applicants' specification).

Narasimhan uses grooves or indentations in the casting wheel to cast a sheet of planar flow cast strip, which has protrusions on one side and corresponding indentations on the other side. Since the depressions in the casting wheel translate at a reduced casting speed, these amorphous sheets with three-dimensional character cannot be laid flat or stacked in any manner to produce a usable stack. Belt cast amorphous sheets might not have these differential velocity problems; but belt casting is not presently used, even in laboratory set-ups, due to severe problems of belt fracture, owing to belt fatigue caused by thermal stresses and repeated bending. It is respectfully submitted that the presence of any indentations in the chill surface of a belt would markedly exasperate these belt fatigue problems. By way of contrast, the strip defined by applicants' claims produces these "articulated topological definitions" by plastically deforming a flat, cast sheet <u>subsequent to the casting operation</u> using heated ribbon or a heated die set. The advantage of using this mode of creating "articulated topological definition", as compared to Narasimhan's method, is that the <u>flatness of the sheet is preserved while maintaining a discontinuity free connection between the</u>

geometrical articulation and the amorphous metal strip. Preservation of sheet flatness, in turn, makes possible the subsequent nesting of strips or lopping off of protrusions to produce a tool. The strips cast on a quench wheel by Narasimhan's process have essentially the curvature of the wheel superimposed thereon; and they cannot be stacked or subject to lopping off operations.

The Narasimhan strip is an 'as-cast' material. As such, it is devoid of any slip lines. By way of contrast the 'articulated topological definition" of strip delineated by applicants' claims is entirely created by plastic deformation, and has slip lines. The magnetic properties of plastically deformed metallic strips are distinctly different from those of as-cast material, since slip lines participate in defining magnetic domain boundaries, and alter the stress state of the laminates. The easy magnetization direction is along the slip bands. [see Amorphous Metallic Alloys Edited by F.E. Luborsky, Butterworths, 1983, pages 313-314, Roll-induced Anisotropy]. Therefore, the "articulated topological definition" required by applicants' claims allows laminated nested cores to be manufactured due to strip flatness. In addition applicants' claimed strip has unique magnetic properties, as compared to Narasimhan's strip, which is not stackable due to the inherent curvature of the strip and has inferior magnetic properties, due to being devoid of slip lines. Accordingly, it is submitted that the Narasimhan product is materially different from that called for by present claims 1-4 and 6-9, and essential geometric and magnetic properties of the Narasimhan product differ significantly from those obtained using the strip called for by applicants' claims 1-4 and 6-9.

These structural elements and magnetic properties clearly distinguish claims 1-4 and 6-9, as amended, from those of conventional as-cast ribbon. Products containing the elements defined by present claims 1-4 and 6-9 are differentiated by the presence of superior mechanical and magnetic properties. In addition, the production of geometrical articulations, as defined by applicants' claims,

results in geometrical articulation of greater magnitude than that obtained by conventional quenching processes while, at the same time, maintaining strip flatness.

Claim 1, as amended, incorporates restrictions on depth of the articulated topographical definition, being greater than strip thickness produced by application of selected forces to introduce permanent deformation on a generally planar previously cast amorphous strip. Claim 1 also requires that the articulated definitions have shape and configuration that is produced without strip embrittelement or crystallization. These restrictions clearly distinguish applicants' strip from that of Narasimhan.

Accordingly, reconsideration of the rejection of Claims 1-4 and 6-9 under 35 U.S.C-102(b) as being anticipated by US Patent 4,332,848 to Narasimhan is respectfully requested.

Claim 5 was rejected under 35 U.S.C. 103(a) as being unpatentable over Narasimhan in view of Watanabe et al. (U.S. Patent 5,622,768) or Sato et al. (U.S. Patent 4,865,664).

The Examiner has stated that Narasimhan products do not appear to contain element "Z" as defined in instant claim 5. The Watanabe or Sato et al patents indicate that it is conventional in the art to include element "Z" in amorphous alloy strip compositions, in the amounts as defined in the instant claim. Consequently, the Watanabe or Sato disclosures would have motivated one of ordinary skill in the art to produce the Narasimhan products containing an amount of element "Z" as defined in the present claims.

As noted hereinabove, the requirements of the alloy called for by claim 5 involve not only quenchability; but also <u>permanent deformation</u> by forces that create the geometrical articulations. Each of Narasimhan, Watanabe and Sato et al. disclose alloys having additions of element "Z" to improve quenchability; but none of these patentees disclose use of the "Z" element to provide superior <u>permanent deformability upon application of force</u>. On the other hand, the amorphous

metal alloy article called for by claim 5, as amended, does <u>not cast</u> geometrically articulated amorphous metal ribbon. Instead, such ribbon is permanently deformed by forces that <u>impress</u> the desired geometrical articulations.

Accordingly, reconsideration of the rejection of Claim 5 under 35 U.S.C. 103(a) as being unpatentable over Narasimhan in view of Watanabe et al or Sato et al is respectfully requested.

Claims 11-13 were rejected under 35 U.S.C. 103(a) as being unpatentable over Narasimhan in view of either Watanabe et a. or Bruckner (U.S Patent 4.853,292).

The Examiner has recognized that Narasimhan does not discuss a plurality of stacked materials or transformer cores, as required by claims 11-13, as amended. However, the Examiner has stated that Both Watanabe and Bruckner indicate it to be conventional in the art to form laminated cores by using a plurality of layers of amorphous metal alloys. Accordingly, it is the Examiner's position that these disclosures would have motivated one of skilled in the art to form the materials disclosed by Narasimhan into the configurations set forth by Watanabe or Bruckner.

Narasimhan discloses as-cast material, which is geometrically articulated by having projections or depressions on a quench surface. Due to the circular or repeating nature of the quench surface only periodic structures are produced; such structures have at least the periodicity of the quench substrate. On the other hand, plastically deformed 3-dimensional shapes of the type required by applicants' claims 11-13, as amended, can be impressed on an amorphous sheet in <u>completely arbitrary</u> non-periodic shapes. An example of a non-periodic geometric articulation is shown in Fig. 3B of applicants' specification. On a quench surface either depressions or projections traverse below the casting nozzle at different casting velocities compared to the general surface of the quench wheel, based on the radius at the projection or depression. Consequently, the depressions are shorter in length compared to the flat portion of the sheet, and the sheet has a

curvature similar to that of the quench wheel. Forcing the amorphous ribbon to a flat shape, generally tears the projections cast. This is of course not a problem with belt casting. Accordingly, flat sheets cast on a quench wheel are not available to produce laminations. Moreover, as previously noted, belt quench casting has been considered impractical, owing to fatigue failure of belt material stemming from high thermal stresses and repeated bending stresses. Such belt fatigue problems are made even more difficult when the belt carries deep depressions. On the other hand, plastically deformed three-dimensional shapes impressed on a planar amorphous sheet can be stacked to produce laminations due to the sheet's lack of fixed curvature. The inherent nature of melt flow during a quench casting process creates severe limitations on the geometry of shapes that can be successfully replicated. This is discussed at col. 1, lines 60 through col. 2, line 17 of Narasimhan. If the angles deviate from the values disclosed by Narasimhan, reproduction of the three-dimensional pattern is not replicated. The geometrically articulated amorphous sheet disclosed by Narasimhan is full of thermal contraction stresses. Such contraction stresses compromise magnetic properties and result in non-uniform stress needed to fracture the sheet, since internal stresses are additive with applied stresses. In order to emphasize the salient features of the present invention, claims 11-13, have been amended to require that the articulated topographical definition be produced by application of selected forces that introduce permanent deformation. The geometrically articulated amorphous product required by claims 11-13, as amended, is inherently different from a sheet composed of as-cast material. The problems of geometry, lack of flatness, inherent periodicity of the quench surface, and thermal contraction stresses discussed hereinabove severely limit the application of geometrically articulated, as-cast amorphous metal sheets. In particular, the magnetic properties, cutting ability and wear resistance of as-cast amorphous metal sheets are severely compromised. These factors differentiate the article delineated by claims 11-13, as amended, from

the cited references. As a result, the geometrically articulated amorphous metal article required by claim 11-13, as amended, exhibits excellent magnetic and mechanical properties, whereas the as-cast amorphous metal alloys disclosed by Narasimhan do not.

Neither Narasimhan nor Watanabe and Bruckner disclose permanently deformed metallic glass strip having macroscopic geometric articulation for laminated cores. Narasimhan's as-cast amorphous material is unsuitable for producing laminated cores, due to several reasons. First, the thermal contraction strains produce poor magnetic properties. Ribbon curvature, inherently produced when the ribbon is cast on a quench wheel, prevents stackability of as-cast, geometrically articulated amorphous metal ribbons. This stackability problem would impair production of an article that comprises a plurality of self-nesting amorphous metal strips, as called for by applicants' claim 11. The material taught by Watanabe et al. and Bruckner has microscopic surface roughness (i.e. no more than .3-30 % of the strip thickness, see col. 2, lines 11-23 of Watanabe et al.), not macroscopic geometric articulations (i.e. greater than the strip thickness, see Figs. 2-4 of applicants' drawings), as required by claims 11-13, as amended. Since the articles produced by Watanabe et al. and Bruckner are as-cast products, they contain thermal contraction strains with poor magnetic properties when laminated. By way of contrast, the article of claims 11 to 13 comprises stackable flat ribbons with geometrical articulation in a relaxed state, thereby providing a self-nesting feature not disclosed or suggested by the art applied. The amendment of claim 11, which requires that the amorphous metal strip be permanently deformed to produce an articulated topographical definition at a depth greater than the strip thickness, distinguishes the subject matter of claims 12 and 13 from the cited references. It also distinguishes the subject matter of claim 11, since geometrical articulations caused by permanent deformation have fixed dimensions each of which are greater than the strip thickness, free from edge burs and other imperfections (which are typically found in

as-cast products). These features significantly improve stackability, thereby enabling articles having articulated topographical definition to be self-nesting.

For the reasons set forth above, it is submitted that combining the Narasimhan product with the laminations disclosed by Watanabe or Bruckner will, of necessity, result in a poorly stacked lamination, since the articulations would not match from strip to strip owing to the inherent curvature of as-cast strip produced on a quench wheel. As previously noted, belt-cast material is essentially non-existent, owing to problems associated with belt material and belt thickness requirements. Large articulations have inherently increased curvature and would not result in a nested lamination, as called for by present claims 11-13. Such a nested lamination stack, and the advantageous features afforded thereby, cannot be obtained unless there is preserved the flatness condition of the strip without melt flow problems inherent to the cast articulated strips with deep structural features produced by Narasimhan.

Accordingly, reconsideration of the rejection of claims 11-13 under 35 U.S.C. 103(a) as being unpateniable over Narasimhan in view of either Watanabe et al or Bruckner (U.S. Patent 4,853,292) is respectfully requested.

In summary, Narasimhan's material is presently produced on a quench wheel exclusively. Troublesome problems associated with belt fatigue -- even with belts devoid of protrusions or indentations – cause <u>belt cast materials to be essentially non-existent</u>. Strips cast on a quench wheel provided with protrusions are <u>inherently non-flat</u> and <u>cannot be stacked or flattened</u>. Narasimhan's as-cast materials are devoid of slip lines, but have <u>large internal quenching stresses</u> that reduce the strip's magnetic properties. By way of contrast, <u>plastic deformation</u> of amorphous magnetic strips called for by applicants' claims results in slip lines; but these slip lines <u>do not impair magnetic properties</u>. Moreover, internal stresses are absent in the plastically deformed, geometrically

articulated material of applicants' claims, which is completely relaxed, thereby providing superior magnetic properties. Further, the articulated topographical definitions of applicants' claimed strip may be periodic, or non-periodic. Such articulated topographical definitions may have any shape or configuration. Still further, with applicants' claimed strip there exists a superior bond between the geometrical articulation and the base strip without presence of the discontinuities inherently contained by Narasimhan's strip. Significantly, the geometrically articulated amorphous material strip delineated by applicants' claims has no restriction on wall angles of articulated topographical definitions. As a result the wall angles of articulated topographical definitions contained by applicants' claimed strip and can approach 90 degrees, thereby packing a large number of articulated topographical definitions per unit area of strip, and providing a superior abrasive surface. The improved bond between geometrical articulations and absence of internal stresses in the strip called for by applicants' claims result in superior abrasive properties.

In view of the amendments to the claims and the remarks set forth above, it is submitted that this application is in allowable condition. Accordingly, reconsideration of the rejection of claims 1-9 and 11-13, as amended, and allowance of the application are earnestly solicited.

Respectfully submitted,
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By: ______________________

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What is claimed is:

1. (Thrice Amended) An amorphous metal alloy strip having an articulated topographical definition of a selected shape or configuration distending at a depth greater than strip thickness produced on a generally planar, previously cast amorphous metal strip by application of selected forces that induce permanent deformation without strip embrittelement or crystallization.

2. (Once Amended) An amorphous metal alloy strip according to claim 1 which comprises a plurality of articulated topographical definitions.

3. (Once Amended) An amorphous metal alloy strip according to claim 1 which comprises a plurality of geometrically repeating articulated topographical definitions.

4. (Once Amended) An amorphous metal alloy strip according to claim 1, having a composition defined by the formula:

$$M_k Y_p$$

wherein:

M is a metal selected from one or more of the group consisting of Fe, Ni, Co, V and Cr;

Y represents one or more elements from the group consisting of P, B and C;

k represents atomic percent, and has a value of from about 70 – 85;

p represents atomic percent, and has a value of about 15 – 30;

5. (Once Amended) An amorphous metal alloy strip according to claim 1, having a composition defined by the formula:

$$M_a Y_b Z_c$$

wherein:

M is a metal selected from one or more of the group consisting of Fe, Ni, Co, V and Cr;

Y represents one or more elements from the group consisting of P, B and C;

Z is one or more elements selected from the group Al, Si, Sn, Ge, In, Sb or Be;

a represents atomic percent and has a value of from about 60 – 90;

b represents atomic percent and has a value of from about 10 – 30;

c represents atomic percent and has a value of from about 0.1 – 15; and, $a+b+c = 100$.

6. (Once Amended) An abrasive article which comprises the amorphous metal alloy strip having an articulated topographical definition according to claim 1.

7. (Once Amended) An abrasive article which comprises amorphous metal alloy strip having a plurality of an articulated topographical definitions according to claim 2.

8. (Once Amended) A cutting article which comprises the amorphous metal alloy strip having an articulated topographical definition according to claim 1.

9. (Once Amended) A cutting article which comprises the amorphous metal alloy strip having a plurality of an articulated topographical definitions according to claim 2.

11. (Twice Amended) An article which comprises a plurality of self-nesting amorphous metal alloy strips, each of said strips being a generally planar, previously cast amorphous metal strip and having an articulated topographical definition of a selected shape or configuration distending at a depth greater than the strip thickness produced thereon by application of selected forces that induce permanent deformation without strip embrittelement or crystallization.

12. (Once Amended) An article according to claim 11, said article being a wound transformer core.

13. (Once Amended) An article according to claim 11, said article being a stacked transformer core.

Amended Claims – Version With Markings To Show Changes Made

What is claimed is:

1. ~~(Twice~~(Thrice Amended) An amorphous metal alloy strip having an articulated topographical definition of a selected shape or configuration distending at a depth greater than strip thickness produced on a generally planar, previously cast amorphous metal strip by application of selected forces that induce permanent deformation without strip embrittelement or crystallization.

2. (Once Amended) An amorphous metal alloy strip according to claim 1 which comprises a plurality of articulated topographical definitions.

3. (Once Amended) An amorphous metal alloy strip according to claim 1 which comprises a plurality of geometrically repeating articulated topographical definitions.

4. (Once Amended) An amorphous metal alloy strip according to claim 1, having a composition defined by the formula:

$$M_k Y_p$$

wherein:

M is a metal selected from one or more of the group consisting of Fe, Ni, Co, V and Cr;

Y represents one or more elements from the group consisting of P, B and C;

k represents atomic percent, and has a value of from about 70 – 85;

p represents atomic percent, and has a value of about 15 – 30;

5. (Once Amended) An amorphous metal alloy strip according to claim 1, having a composition defined by the formula:

$$M_a Y_b Z_c$$

wherein:

M is a metal selected from one or more of the group consisting of Fe, Ni, Co, V and Cr;

Y represents one or more elements from the group consisting of P, B and C;

Z is one or more elements selected from the group Al, Si, Sn, Ge, In, Sb or Be;

a represents atomic percent and has a value of from about 60 – 90;

b represents atomic percent and has a value of from about 10 – 30;

c represents atomic percent and has a value of from about 0.1 – 15; and, a+b+c = 100.

6. (<u>Once</u> Amended) An abrasive article which comprises the amorphous metal alloy strip having an articulated topographical definition according to claim 1.

7. (<u>Once</u> Amended) An abrasive article which comprises amorphous metal alloy strip having a plurality of an articulated topographical definitions according to claim 2.

8. (<u>Once</u> Amended) A cutting article which comprises the amorphous metal alloy strip having an articulated topographical definition according to claim 1.

9. (<u>Once</u> Amended) A cutting article which comprises the amorphous metal alloy strip having a plurality of an articulated topographical definitions according to claim 2.

11. (<u>Twice</u> Amended) An article which comprises a plurality of self-nesting amorphous metal alloy strips, each of said strips being a generally planar, <u>previously</u> cast amorphous metal strip and having an articulated topographical definition <u>of a selected shape or configuration distending</u> at a depth greater than the strip thickness produced thereon by application of selected forces that induce permanent deformation <u>without strip embrittelement or crystallization</u>.

12. (<u>Once</u> Amended) An article according to claim 11, said article being a wound transformer core.

13. (<u>Once</u> Amended) An article according to claim 11, said article being a stacked transformer core.